APPENDIX D PCAPCD EMISSION CALCULATIONS

PCAPCD EMISSION CALCULATIONS FOR GE LM6000 OPTION

| NOx only - Possible operating scenario - GE LM6000 Option | | | | | | | |
|---|-------|-------|-------|-------|-------|--|--|
| 140x only - I ossible operating s | 1st | 2nd | 3rd | 4th | | | |
| Base Load Only Hours | 1,324 | 1,094 | 1,247 | 1,298 | 4,963 | | |
| Peaking Hours (Duct Firing) | 500 | 321 | 849 | 509 | 2,179 | | |
| Total Base and Peak Hours | 1,824 | 1,415 | 2,096 | 1,807 | 7,142 | | |
| Total Startup Hours | 50 | 83 | 26 | 52 | 211 | | |
| Total Operating Hours | 1,874 | 1,498 | 2,122 | 1,859 | 7,353 | | |
| Offline Hours | 286 | 686 | 86 | 350 | 1,408 | | |
| Total Hours in Period | 2,160 | 2,184 | 2,208 | 2,208 | 8,760 | | |
| Capacity Factor | | | | | | | |
| Base Load | 84% | 65% | 95% | 82% | 82% | | |
| Peaking | 23% | 15% | 38% | 23% | 25% | | |
| Weighted (approx.) | 68% | 51% | 80% | 66% | 66% | | |
| Number of Hours of Starts (each CTG) | | | | | | | |
| Hot | 14.0 | 31.0 | 23.0 | 19.0 | 87.0 | | |
| Warm | 16.5 | 19.5 | 1.0 | 12.0 | 49.0 | | |
| Cold | 1.0 | 4.3 | 0.3 | 3.0 | 8.7 | | |
| Total Number of Hours of Starts | 31.5 | 54.8 | 24.3 | 34.0 | 144.7 | | |
| Hours per Start | | | | | | | |
| Hot | _ 1 | | | | | | |
| Warm | 2 | | | | | | |
| Cold | 3 | | | | | | |

Hours Hours Hours Hours Quarter 1 Quarter 2 Quarter 3 Quarter 4 1,943 1,589 2,127 1,916

| | | Quarter | | | Total |
|-----------------------------|-----------------|-----------------|-----------------|-----------------|--------|
| | Q uarter | | | | |
| Element/Operation | 1 st | 2 nd | 3 rd | 4 th | Annual |
| Power Plant: | | | | | |
| Base load only | 1,123 | 1,188 | 751 | 852 | 3,91 |
| hours | | | | | |
| Peaking hours (duct firing) | 929 | 559 | 1,347 | 1,246 | 4,08 |
| Total base and peak | 2,052 | 1,747 | 2,098 | 2,098 | 7,99 |
| hours | | | | | |
| Total startup hours | 44 | 127 | 34 | 47 | 25 |
| Total operating | 2,096 | 1,874 | 2,132 | 2,145 | 8,24 |
| hours | | | | | |
| Offline hours | 64 | 310 | 76 | 63 | 51 |
| Total hours in period | 2,160 | 2,184 | 2,208 | 2,208 | 8,76 |
| Capacity factor: | | | | | |
| Base load | 95% | 80% | 95% | 95% | 919 |
| Peaking | 43% | 26% | 61% | 56% | 479 |
| Weighted (approximately) | 81% | 65% | 86% | 85% | 799 |
| Hours of starts (each CTG): | | | | | |
| Hot | 25 | 71 | 29 | 42 | 16 |
| Warm | 8 | 20 | 1 | 1 | 3 |
| Cold | 1 | 2 | 1 | 1 | |
| Total number of | 34 | 98 | 31 | 44 | 20 |
| Hours of starts | | | | | |
| Hours per start | | | | | |
| Hot | 1 | | | | |
| Warm | 2 | | | | |
| Cold | 3 | | | | |
| Auxiliary boiler: | | | | | |
| Margin | 30% | | | | |
| Operating hours | 140 | 568 | 143 | 143 | 99 |
| Standby generator: | | | | | |
| Number of Tests | 25 | 25 | 25 | 25 | 10 |
| Fire pump: | | | | | |
| Number of Tests | 25 | 25 | 25 | 25 | 10 |

GE LM6000 Turbines

| BASE | lbs/hr per turbine | lbs/hr two turbines | Hours/turbine Quarter 1 | Hours/turbine Quarter 2 | Hours/turbine Quarter 3 | Hours/turbine Quarter 4 |
|------|--------------------------|---------------------------|----------------------------|----------------------------|----------------------------|----------------------------|
| NOx | 3.408 | 6.816 | 1,324 | 1,094 | 1,247 | 1,298 |
| CO | 4.15 | 8.3 | 1,123 | 1,188 | 751 | 852 |
| VOC | 1.188 | 2.376 | 1,123 | 1,188 | 751 | 852 |
| PM10 | 3.166 | 6.332 | 1,123 | 1,188 | 751 | 852 |
| SO2 | 0.657 | 1.314 | 1,123 | 1,188 | 751 | 852 |

| PEAK | lbs/hr per turbine | lbs/hr two turbines | Hours Quarter 1 | Hours Quarter 2 | Hours Quarter 3 | Hours Quarter 4 |
|------|--------------------------|---------------------------|--------------------|--------------------|--------------------|--------------------|
| NOx | 4.994 | 9.988 | 500 | 321 | 849 | 509 |
| CO | 6.081 | 12.162 | 929 | 559 | 1,347 | 1,246 |
| VOC | 1.742 | 3.484 | 929 | 559 | 1,347 | 1,246 |
| PM10 | 4.617 | 9.234 | 929 | 559 | 1,347 | 1,246 |
| SO2 | 0.959 | 1.918 | 929 | 559 | 1,347 | 1,246 |

| HOT START | lbs/hr per turbine | lbs/hr two turbines | Hot Start Hours Quarter 1 | Hot Start Hours Quarter 2 | Hot Start Hours Quarter 3 | Hot Start Hours Quarter 4 |
|--------------|--------------------------|---------------------------|---------------------------------|---------------------------------|------------------------------|---------------------------------|
| NOx | 8.8 | 15.9 | 14 | 31 | 23 | 19 |
| CO | 9.2 | 16.3 | 25 | 71 | 29 | 42 |
| VOC | 1.4 | 2.3 | 25 | 71 | 29 | 42 |
| PM10 | 3.2 | 6.3 | 25 | 71 | 29 | 42 |
| SO2 | 0.7 | 1.3 | 25 | 71 | 29 | 42 |

| WARM START | lbs/hr per turbine | lbs/hr two turbines | Warm Start Hours Quarter 1 | Warm Start Hours Quarter 2 | Warm Start Hours Quarter 3 | Warm Start Hours Quarter 4 |
|---------------|--------------------------|---------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|
| NOx | 12.2 | 29.2 | 33 | 39 | 2 | 24 |
| CO | 10.8 | 27.6 | 8 | 20 | 1 | 1 |
| VOC | 1.4 | 4.5 | 8 | 20 | 1 | 1 |
| PM10 | 3.2 | 12.7 | 8 | 20 | 1 | 1 |
| SO2 | 0.7 | 2.6 | 8 | 20 | 1 | 1 |

| COLD START | lbs/hr per turbine | lbs/hr two turbines | Cold Start Hours Quarter 1 | Cold Start Hours Quarter 2 | Cold Start Hours Quarter 3 | Cold Start Hours Quarter 4 |
|---------------|--------------------------|---------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|
| NOx | 19.3 | 49.7 | 3 | 13 | 1 | 9 |
| CO | 14.3 | 42.2 | 1 | 2 | 1 | 1 |
| VOC | 1.4 | 6.6 | 1 | 2 | 1 | 1 |
| PM10 | 3.2 | 19 | 1 | 2 | 1 | 1 |
| SO2 | 0.7 | 3.9 | 1 | 2 | 1 | 1 |

GE LM6000 Turbines

| BASE | Lbs/quarter per turbine Quarter 1 | Lbs/quarter per turbine Quarter 2 | Lbs/quarter per turbine Quarter 3 | Lbs/quarter per turbine Quarter 4 |
|-----------|---|---|-----------------------------------|-----------------------------------|
| NO_x | 4,512 | 3,728 | 4,250 | 4,422 |
| co | 4,660 | 4,930 | 3,117 | 3,536 |
| VOC | 1,334 | 1,411 | 892 | 1,012 |
| PM_{10} | 3,555 | 3,761 | 2,378 | 2,697 |
| SO_2 | 738 | 781 | 493 | 560 |

| PEAK | Lbs/quarter per turbine Quarter 1 | Lbs/quarter per turbine Quarter 2 | Lbs/quarter per turbine Quarter 3 | Lbs/quarter per turbine Quarter 4 |
|-----------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|
| NO_x | 2,497 | 1,603 | 4,240 | 2,542 |
| СО | 5,649 | 3,399 | 8,191 | 7,577 |
| VOC | 1,618 | 974 | 2,346 | 2,171 |
| PM_{10} | 4,289 | 2,581 | 6,219 | 5,753 |
| SO_2 | 891 | 536 | 1,292 | 1,195 |

| HOT START | Lbs/quarter per turbine Quarter 1 | Lbs/quarter per turbine Quarter 2 | Lbs/quarter per turbine Quarter 3 | Lbs/quarter per turbine Quarter 4 |
|--------------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|
| NO_x | 123 | 273 | 202 | 167 |
| СО | 230 | 653 | 267 | 386 |
| VOC | 35 | 99 | 41 | 59 |
| PM_{10} | 80 | 227 | 93 | 134 |
| SO_2 | 18 | 50 | 20 | 29 |

| WARM START | Lbs/quarter per turbine Quarter 1 | Lbs/quarter per turbine Quarter 2 | Lbs/quarter per turbine Quarter 3 | Lbs/quarter per turbine Quarter 4 |
|---------------|---|-----------------------------------|-----------------------------------|-----------------------------------|
| NO_x | 403 | 476 | 24 | 293 |
| CO | 86 | 216 | 11 | 11 |
| VOC | 11 | 28 | 1 | 1 |
| PM_{10} | 26 | 64 | 3 | 3 |
| SO_2 | 6 | 14 | 1 | 1 |

| COLD START | Lbs/quarter per turbine Quarter 1 | Lbs/quarter per turbine Quarter 2 | Lbs/quarter per turbine Quarter 3 | Lbs/quarter per turbine Quarter 4 |
|---------------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|
| NO_x | 58 | 251 | 19 | 174 |
| СО | 14 | 29 | 14 | 14 |
| VOC | 1 | 3 | 1 | 1 |
| PM_{10} | 3 | 6 | 3 | 3 |
| SO_2 | 1 | 1 | 1 | 1 |

GE LM6000 Turbines

| BASE | Two Turbine Base Quarter 1 Lbs/quarter | Two Turbine Base Quarter 2 Lbs/quarter | Two Turbine Base Quarter 3 Lbs/quarter | Two Turbine Base Quarter 4 Lbs/quarter | Annual (Tpy) |
|-----------------|---|---|--|---|--------------|
| NO_x | 9,024 | 7,457 | 8,500 | 8,844 | 16.91 |
| CO | 9,321 | 9,860 | 6,233 | 7,072 | 16.24 |
| VOC | 2,668 | 2,823 | 1,784 | 2,024 | 4.65 |
| PM_{10} | 7,111 | 7,522 | 4,755 | 5,395 | 12.39 |
| SO ₂ | 1,476 | 1,561 | 987 | 1,120 | 2.57 |

| PEAK | Two Turbine Peak Quarter 1 Lbs/quarter | Two Turbine Peak Quarter 2 Lbs/quarter | Two Turbine Peak Quarter 3 Lbs/quarter | Two Turbine Peak Quarter 4 Lbs/quarter | Annual (Tpy) |
|------------------|---|---|--|---|--------------|
| NO_x | 4,994 | 3,206 | 8,480 | 5,084 | 10.88 |
| CO | 11,298 | 6,799 | 16,382 | 15,154 | 24.82 |
| VOC | 3,237 | 1,948 | 4,693 | 4,341 | 7.11 |
| PM ₁₀ | 8,578 | 5,162 | 12,438 | 11,506 | 18.84 |
| SO ₂ | 1,782 | 1,072 | 2,584 | 2,390 | 3.91 |

| HOT START | Two Turbine Hot Start Quarter 1 Lbs/quarter | Two Turbine Hot Start Quarter 2 Lbs/quarter | | Two Turbine Hot Start | Annual (Tpy) | |
|-----------|--|--|-----|-----------------------|--------------|----|
| NO_x | 223 | 493 | 366 | 302 | 0.6 | 69 |
| CO | 408 | 1,157 | 473 | 685 | 1.3 | 36 |
| VOC | 58 | 163 | 67 | 97 | 0.1 | 19 |
| PM_{10} | 158 | 447 | 183 | 265 | 0.5 | 53 |
| SO_2 | 33 | 92 | 38 | 55 | 0.1 | 11 |

| WARM START | Two Turbine Warm Start Quarter 1 Lbs/quarter | Two Turbine Warm Start Quarter 2 Lbs/quarter | Two Turbine Warm Start Quarter 3 Lbs/quarter | Two Turbine Warm Start Quarter 4 Lbs/quarter | Annual (Tpy) |
|------------|---|--|---|---|--------------|
| NO_x | 964 | 1,139 | 58 | 701 | 1.43 |
| CO | 221 | 552 | 28 | 28 | 0.41 |
| VOC | 36 | 90 | 5 | 5 | 0.07 |
| PM_{10} | 102 | 254 | 13 | 13 | 0.19 |
| SO_2 | 21 | 52 | 3 | 3 | 0.04 |

| COLD START | Two Turbine Cold Start Quarter 1 Lbs/quarter | Two Turbine Cold start Quarter 2 Lbs/quarter | Two Turbine Cold Start Quarter 3 Lbs/quarter | Two Turbine Cold Start Quarter 4 Lbs/quarter | |
|------------|---|--|--|---|------|
| NO_x | 149 | 646 | 50 | 447 | 0.65 |
| CO | 42 | 84 | 42 | 42 | 0.11 |
| VOC | 7 | 13 | 7 | 7 | 0.02 |
| PM_{10} | 19 | 38 | 19 | 19 | 0.05 |
| SO_2 | 4 | 8 | 4 | 4 | 0.01 |

| STARTUP SUBTOTAL | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|------------------|-----------|-----------|-----------|-----------|--------------|
| NO _x | 1,335 | 2,278 | 474 | 1,450 | 2.77 |
| CO | 671 | 1,794 | 543 | 754 | 1.88 |
| VOC | 100 | 267 | 78 | 108 | 0.28 |
| PM_{10} | 278 | 739 | 214 | 296 | 0.76 |
| SO_2 | 57 | 152 | 44 | 61 | 0.16 |

| TURBINE TOTAL | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|---------------|-----------|-----------|-----------|-----------|--------------|
| NO_x | 15,354 | 12,941 | 17,453 | 15,378 | 30.56 |
| CO | 21,290 | 18,453 | 23,158 | 22,980 | 42.94 |
| VOC | 6,005 | 5,037 | 6,555 | 6,473 | 12.03 |
| PM_{10} | 15,967 | 13,424 | 17,408 | 17,197 | 32.00 |
| SO_2 | 3,315 | 2,785 | 3,615 | 3,570 | 6.64 |

| GE CTG and HRSG | lbs/hr | lbs/day | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|--------------------|--------|---------|-----------|-----------|-----------|-----------|--------------|
| NOx | | | 15,354 | 12,941 | 17,453 | 15,378 | 30.56 |
| CO | | | 21,290 | 18,453 | 23,158 | 22,980 | 42.94 |
| VOC | | | 6,005 | 5,037 | 6,555 | 6,473 | 12.03 |
| PM10 | | | 15,967 | 13,424 | 17,408 | 17,197 | 32.00 |
| SO2 | | | 3,315 | 2,785 | 3,615 | 3,570 | 6.64 |

| BOILER | lbs/hr | lbs/day | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|--------|--------|---------|-----------|-----------|-----------|-----------|--------------|
| NOx | 0.68 | 16.3 | 95 | 386 | 97 | 97 | 0.34 |
| CO | 2.29 | 55.0 | 321 | 1301 | 327 | 327 | 1.14 |
| VOC | 0.31 | 7.5 | 44 | 177 | 44 | 44 | 0.15 |
| PM10 | 0.58 | 13.9 | 81 | 329 | 83 | 83 | 0.29 |
| SO2 | 0.08 | 1.9 | 11 | 45 | 11 | 11 | 0.04 |

| Cooling Tower | lbs/hr | lbs/day | | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|---------------|--------|---------|---|-----------|-----------|-----------|-----------|--------------|
| | | | | | | | | |
| NOx | - | - | - | | | | | |
| CO | - | - | - | | | | | |
| VOC | - | - | - | | | | | |
| PM10 | 0.681 | 16.35 | | 1,471 | 1,487 | 1,504 | 1,504 | 2.98 |
| SO2 | - | - | - | | | | | |

| ТОТ | TOTAL EMISSIONS - Boiler, GE Turbines, Cooling Tower | | | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|------|--|--|--------|-----------|-----------|-----------|--------------|
| | | | | | | | |
| NOx | | | 15,449 | 13,327 | 17,550 | 15,475 | 30.90 |
| CO | | | 21,610 | 19,753 | 23,485 | 23,307 | 44.08 |
| VOC | | | 6,049 | 5,213 | 6,600 | 6,518 | 12.19 |
| PM10 | | | 17,520 | 15,240 | 18,995 | 18,783 | 35.27 |
| SO2 | | | 3,326 | 2,831 | 3,626 | 3,582 | 6.68 |

| Emergency C | Generator (Caterp | illar , | 1133 | hp | | | | |
|--------------------|-------------------|---------|---------------------------|-----------|-----------|-----------|-----------|--------------|
| | g/hp-hr | lbs/hr | lbs/day (1/2 hour max) | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
| NOx | 6.9 | 4.31 | 4.31 | 54 | 54 | 54 | 54 | 0.108 |
| CO | 1.34 | 0.84 | 0.84 | 10 | 10 | 10 | 10 | 0.021 |
| VOC | 0.25 | 0.16 | 0.16 | 2 | 2 | 2 | 2 | 0.004 |
| PM10 | 0.22 | 0.14 | 0.14 | 2 | 2 | 2 | 2 | 0.003 |
| SO2 | - | 0.10 | 0.10 | 1 | 1 | 1 | 1 | 0.002 |

Assuming 30 minutes per week testing (12.5 hours/quarter) and total of 50 hrs per year max at 50% load.

Daily maximum calculated based on 30 minutes testing. Quarterly emissions calculated based on 12.5 hours per quarter.

| 300.0 hp | | | | | | | |
|----------|-----------------------------|---|--|---|--|---|--|
| g/hp-hr | lbs/hr | lbs/day (1/2 hour max) | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
| 5.2 | 1.72 | 1.72 | 43 | 43 | 43 | 43 | 0.086 |
| 0.27 | 0.09 | 0.09 | 2 | 2 | 2 | 2 | 0.004 |
| 0.15 | 0.05 | 0.05 | 1 | 1 | 1 | 1 | 0.002 |
| 0.09 | 0.03 | 0.03 | 1 | 1 | 1 | 1 | 0.001 |
| 0.099 | 0.19 | 0.19 | 5 | 5 | 5 | 5 | 0.010 |
| | 5.2 0.27 0.15 0.09 | 5.2 1.72 0.27 0.09 0.15 0.05 0.09 0.03 | g/hp-hr lbs/hr lbs/day (1/2 hour max) 5.2 1.72 1.72 0.27 0.09 0.09 0.15 0.05 0.05 0.09 0.03 0.03 | g/hp-hr lbs/hr lbs/day (1/2 hour max) Quarter 1 5.2 1.72 1.72 43 0.27 0.09 0.09 2 0.15 0.05 0.05 1 0.09 0.03 0.03 1 | g/hp-hr lbs/hr lbs/day (1/2 hour max) Quarter 1 Quarter 2 5.2 1.72 1.72 43 43 0.27 0.09 0.09 2 2 0.15 0.05 0.05 1 1 0.09 0.03 0.03 1 1 | g/hp-hr lbs/hr lbs/day (1/2 hour max) Quarter 1 Quarter 2 Quarter 3 5.2 1.72 1.72 43 43 43 0.27 0.09 0.09 2 2 2 0.15 0.05 0.05 1 1 1 0.09 0.03 0.03 1 1 1 | g/hp-hr lbs/hr lbs/day (1/2 hour max) Quarter 1 Quarter 2 Quarter 3 Quarter 4 5.2 1.72 1.72 43 43 43 43 0.27 0.09 0.09 2 2 2 2 0.15 0.05 0.05 1 1 1 1 0.09 0.03 0.03 1 1 1 1 |

Assuming 30 minutes per week testing (12.5 hours/quarter) and total of 50 hrs per year max at 100% load.

Daily maximum calculated based on 30 minutes testing. Quarterly emissions calculated based on 12.5 hours per quarter.

| Total Facility - GE LM6000 Turbines | | | | | | | |
|-------------------------------------|-----|--------|-----------|-----------|-----------|--------------|--|
| | Qua | ter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) | |
| NOx | | 5,546 | 13,424 | 17,647 | 15,572 | 31.09 | |
| CO | | 21,623 | 19,766 | 23,498 | 23,320 | 44.10 | |
| VOC | | 6,052 | 5,217 | 6,603 | 6,521 | 12.20 | |
| PM10 | | 7,522 | 15,243 | 18,997 | 18,786 | 35.27 | |
| SO2 | | 3,332 | 2,837 | 3,632 | 3,588 | 6.69 | |

PCAPCD EMISSION CALCULATIONS FOR ALSTOM GX-100 OPTION

| NOx only - Possible operating | scenario - A | 2nd | 3rd | 4th | |
|--------------------------------------|--------------|---------|---------|---------|---------|
| Base Load Only Hours | 1,124.9 | 833.2 | 1,179.4 | 1,102.7 | 4,240.2 |
| Peaking Hours (Duct Firing) | 424.8 | 244.5 | 803.0 | 432.6 | 1,904.9 |
| Total Base and Peak Hours | 1,549.7 | 1,077.7 | 1,982.4 | 1,535.3 | 6,145.1 |
| Total Startup Hours | 42.5 | 63.2 | 24.6 | 44.2 | 174.5 |
| Total Operating Hours | 1,592.2 | 1,140.9 | 2,007.0 | 1,579.5 | 6,319.6 |
| Offline Hours | 567.8 | 1,043.1 | 201.0 | 628.5 | 2,440.4 |
| Total Hours in Period | 2,160.0 | 2,184.0 | 2,208.0 | 2,208.0 | 8,760.0 |
| Capacity Factor | | | | | |
| Base Load | 0.7 | 0.5 | 0.9 | 0.7 | 0.7 |
| Peaking | 0.2 | 0.1 | 0.4 | 0.2 | 0.2 |
| Weighted (approx.) | 0.6 | 0.4 | 0.8 | 0.6 | 0.6 |
| Number of Hours of Starts (each CTG) | | | | | |
| Hot | 11.9 | 23.6 | 21.8 | 16.1 | 73.4 |
| Warm | 14.0 | 14.9 | 0.9 | 10.2 | 40.0 |
| Cold | 0.8 | 3.3 | 0.3 | 2.5 | 7.0 |
| Total Number of Hours of Starts | 26.8 | 41.8 | 23.0 | 28.9 | 120.4 |
| Hours per Start | | | | | |
| Hot | 1.0 | | | | |
| Warm | 2.0 | | | | |
| Cold | 3.0 | | | | |

Turbine including startup/shutdown TOTAL HOURS

Hours Hours Hours Hours Quarter Quarter Quarter 1 2 3 4 1,651 1,210 2,012 1,628

| ant dispatch schedule CO, PM-10, SOX and VOCs - Alstom GX-100 Option | | | | | | |
|--|-----------------|-----------------|-----------------|---|--------|--|
| | Quarter Total | | | | | |
| | 1 st | 2 nd | 3 rd | 4 th | Annual | |
| Element/Operation Power Plant: | | | ა | 4 | Annual | |
| | 1,123 | 1,188 | 751 | 852 | 3,914 | |
| Base load only hours | 1,123 | 1,100 | 731 | 632 | 3,914 | |
| Peaking hours (duct firing) | 929 | 559 | 1,347 | 1,246 | 4,081 | |
| | | | | | | |
| Total base and peak hours | 2,052 | 1,747 | 2,098 | 2,098 | 7,995 | |
| Total startup hours | 44 | 127 | 34 | 47 | 252 | |
| Total startap nours | 11 | 127 | 31 | 1, | 232 | |
| Total operating hours | 2,096 | 1,874 | 2,132 | 2,145 | 8,247 | |
| | | | | | | |
| Offline hours | 64 | 310 | 76 | 63 | 513 | |
| Total hours in period | 2,160 | 2,184 | 2,208 | 2,208 | 8,760 | |
| Capacity factor: | | | | | | |
| Base load | 95% | 80% | 95% | 95% | 91% | |
| Peaking | 43% | 26% | 61% | 56% | 47% | |
| <u>. </u> | 81% | 65% | | 85% | 79% | |
| Weighted (approximately) | 81% | 03% | 86% | 83% | 19% | |
| Hours of starts (each CTG): | | | | | | |
| Hot | 25 | 71 | 29 | 42 | 167 | |
| Warm | 8 | 20 | 1 | 1 | 30 | |
| Cold | 1 | 2 | 1 | 1 | 5 | |
| Total number of Hours of starts | 34 | 98 | 31 | 44 | 207 | |
| House por stort | | | | | | |
| Hours per start Hot | 1 | | | | | |
| | | | | | | |
| Warm Cold | 2 3 | | | | | |
| Auxiliary boiler: | 3 | | | | | |
| • | 200/ | | | | | |
| Margin | 30% | 5 (0) | 1.40 | 1.40 | 005 | |
| Operating hours | 140 | 568 | 143 | 143 | 995 | |
| Standby generator: | | | | · | | |
| Number of Tests | 25 | 25 | 25 | 25 | 100 | |
| Fire pump: | | | | ••••••••••••••••••••••••••••••••••••••• | | |
| Number of Tests | 25 | 25 | 25 | 25 | 100 | |

PCAPCD Emission Calculations Alstom GX100 Turbines

| BASE | lbs/hr per turbine | lbs/hr two turbines | Hours/turbine Quarter 1 | Hours/turbine Quarter 2 | Hours/turbine Quarter 3 | Hours/turbine Quarter 4 |
|-----------|-----------------------|---------------------------|----------------------------|----------------------------|----------------------------|----------------------------|
| NO_x | 3.469 | 6.938 | 1,125 | 833 | 1,179 | 1,103 |
| СО | 4.224 | 8.448 | 1123 | 1188 | 751 | 852 |
| VOC | 0.363 | 0.730 | 1123 | 1188 | 751 | 852 |
| PM_{10} | 3.222 | 6.444 | 1123 | 1188 | 751 | 852 |
| SO_2 | 0.669 | 1.338 | 1123 | 1188 | 751 | 852 |

| PEAK | lbs/hr per turbine | lbs/hr two turbines | Hours Quarter 1 | Hours Quarter 2 | Hours Quarter 3 | Hours Quarter 4 |
|-----------|-----------------------|---------------------|--------------------|--------------------|--------------------|--------------------|
| NO_x | 5.133 | 10.266 | 424.8 | 244.4736 | 802.9842 | 432.5991 |
| со | 6.226 | 12.452 | 929 | 559 | 1347 | 1246 |
| VOC | 1.783 | 3.566 | 929 | 559 | 1347 | 1246 |
| PM_{10} | 4.726 | 9.452 | 929 | 559 | 1347 | 1246 |
| SO_2 | 0.981 | 1.962 | 929 | 559 | 1347 | 1246 |

| HOT START | Pounds Per Start - one turbine | Pounds Per Start - two turbines | Hot Start Hours Quarter 1 | Hot Start Hours Quarter 2 | Hot Start Hours Quarter 3 | Hot Start Hours Quarter 4 |
|-----------------|--------------------------------|---------------------------------|---------------------------------|---------------------------------|---------------------------------|---------------------------------|
| NO _x | 22.6 | 34.1 | 12 | 24 | . 22 | 16 |
| СО | 83.5 | 160.8 | 25 | 71 | 29 | 42 |
| VOC | 19.6 | 38.8 | 25 | 71 | 29 | 42 |
| PM_{10} | 3.2 | 6.4 | 25 | 71 | 29 | 42 |
| SO ₂ | 0.7 | 1.3 | 25 | 71 | 29 | 42 |

| | | Pounds | Pounds | | | | |
|-----------|------------|-------------|-----------|------------|------------|------------|------------|
| | | Per Start - | Per Start | Warm Start | Warm Start | Warm Start | Warm Start |
| | | one | - two | Hours | Hours | Hours | Hours |
| | WARM START | turbine | turbines | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 |
| NO_x | | 37.1 | 88.1 | 28 | 30 | 2 | 20 |
| СО | | 89.5 | 188.1 | 8 | 20 | 1 | 1 |
| VOC | | 19.7 | 76.7 | 8 | 20 | 1 | 1 |
| PM_{10} | | 3.2 | 12.9 | 8 | 20 | 1 | 1 |
| SO_2 | | 0.7 | 2.7 | 8 | 20 | 1 | 1 |

| | Pounds | Pounds | | | | |
|------------|-------------|-----------|------------|------------|------------|------------|
| | Per Start - | Per Start | Cold Start | Cold Start | Cold Start | Cold Start |
| | one | - two | Hours | Hours | Hours | Hours |
| COLD START | turbine | turbines | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 |
| NO_x | 37.1 | 122.8 | 3 | 10 | 1 | 8 |
| со | 89.5 | 204.8 | 1 | 2 | 1 | 1 |
| voc | 19.7 | 78.6 | 1 | 2 | 1 | 1 |
| PM_{10} | 3.2 | 19.3 | 1 | 2 | 1 | 1 |
| SO_2 | 0.7 | 4 | 1 | 2 | 1 | 1 |

Alstom GX100 Turbines

| BASE | Lbs/quarter per turbine Quarter 1 | | per turbine | per turbine |
|-----------|---|-------|-------------|-------------|
| NO_x | 3,902 | 2,890 | 4,091 | 3,825 |
| CO | 4,744 | 5,018 | 3,172 | 3,599 |
| VOC | 408 | 431 | 273 | 309 |
| PM_{10} | 3,618 | 3,828 | 2,420 | 2,745 |
| SO_2 | 751 | 795 | 502 | 570 |

| PEAK | Lbs/quarter per turbine Quarter 1 | per turbine | per turbine | per turbine |
|-----------|---|-------------|-------------|-------------|
| NO_x | 2,180 | 1,255 | 4,122 | 2,221 |
| CO | 5,784 | 3,480 | 8,386 | 7,758 |
| VOC | 1,656 | 997 | 2,402 | 2,222 |
| PM_{10} | 4,390 | 2,642 | 6,366 | 5,889 |
| SO_2 | 911 | 548 | 1,321 | 1,222 |

| HOT START | | per turbine | per turbine | per turbine |
|--------------|-------|-------------|-------------|-------------|
| NO_x | 269 | 534 | 492 | 365 |
| CO | 2,088 | 5,929 | 2,422 | 3,507 |
| VOC | 490 | 1,392 | 568 | 823 |
| PM_{10} | 80 | 227 | 93 | 134 |
| SO_2 | 18 | 50 | 20 | 29 |

| WARM START | | per turbine | per turbine | per turbine |
|---------------|-------|-------------|-------------|-------------|
| NO_x | 1,040 | 1,102 | 70 | 757 |
| CO | 716 | 1,790 | 90 | 90 |
| VOC | 158 | 394 | 20 | 20 |
| PM_{10} | 26 | 64 | 3 | 3 |
| SO_2 | 6 | 14 | 1 | 1 |

| COLD START | • | | per turbine | per turbine |
|---------------|-----|-----|-------------|-------------|
| NO, | 95 | 367 | 35 | 284 |
| CO | 90 | 179 | 90 | 90 |
| VOC | 20 | 39 | 20 | 20 |
| PM_{10} | 3 | 6 | 3 | 3 |
| SO | . 1 | 1 | 1 | 1 |

Alstom GX100 Turbines

| BASE | Two Turbine Base Quarter 1 Lbs/quarter | Two Turbine Base Quarter 2 Lbs/quarter | Two Turbine Base Quarter 3 Lbs/quarter | Two Turbine Base Quarter 4 Lbs/quarter | Annual (Tpy) |
|-----------------|--|--|--|--|--------------|
| NO_x | 7,804 | 5,781 | 8,183 | 7,651 | 14.71 |
| CO | 9,487 | 10,036 | 6,344 | 7,198 | 16.53 |
| VOC | 815 | 862 | 545 | 619 | 1.42 |
| PM_{10} | 7,237 | 7,655 | 4,839 | 5,490 | 12.61 |
| SO ₂ | 1,503 | 1,590 | 1,005 | 1,140 | 2.62 |

| PEAK | Two Turbine Peak Quarter 1 Lbs/quarter | Two Turbine Peak Quarter 2 Lbs/quarter | Two Turbine Peak Quarter 3 Lbs/quarter | Two Turbine Peak Quarter 4 Lbs/quarter | Annual (Tpy) |
|-----------|--|--|--|--|--------------|
| NO_x | 4,361 | 2,510 | 8,243 | 4,441 | 9.78 |
| CO | 11,568 | 6,961 | 16,773 | 15,515 | 25.41 |
| VOC | 3,313 | 1,993 | 4,803 | 4,443 | 7.28 |
| PM_{10} | 8,781 | 5,284 | 12,732 | 11,777 | 19.29 |
| SO_2 | 1,823 | 1,097 | 2,643 | 2,445 | 4.00 |

| HOT START | Two Turbine Hot Start Quarter 1 Lbs/quarter | Two Turbine Hot Start Quarter 2 Lbs/quarter | Two Turbine Hot Start Quarter 3 Lbs/quarter | Start Quarter 4 | Annual (Tpy) |
|-----------|---|---|---|-----------------|--------------|
| NO_x | 406 | 805 | 742 | 551 | 1.25 |
| CO | 4,020 | 11,417 | 4,663 | 6,754 | 13.43 |
| VOC | 970 | 2,755 | 1,125 | 1,630 | 3.24 |
| PM_{10} | 160 | 454 | 186 | 269 | 0.53 |
| SO_2 | 33 | 92 | 38 | 55 | 0.11 |

| WARM START | Two Turbine Warm Start Quarter 1 Lbs/quarter | Two Turbine Warm Start Quarter 2 Lbs/quarter | Two Turbine Warm Start Quarter 3 Lbs/quarter | Two Turbine Warm Start Quarter 4 Lbs/quarter | Annual (Tpy) |
|------------|---|---|---|---|--------------|
| NO_x | 2,470 | 2,617 | 167 | 1,797 | 3.53 |
| CO | 1,505 | 3,762 | 188 | 188 | 2.82 |
| VOC | 614 | 1,534 | 77 | 77 | 1.15 |
| PM_{10} | 103 | 258 | 13 | 13 | 0.19 |
| SO_2 | 22 | 54 | 3 | 3 | 0.04 |

| COLD START | Two Turbine Cold Start Quarter 1 Lbs/quarter | Two Turbine Cold start Quarter 2 Lbs/quarter | Two Turbine Cold Start Quarter 3 Lbs/quarter | Two Turbine Cold Start Quarter 4 Lbs/quarter | |
|------------|--|--|---|---|------|
| NO_x | 313 | 1,216 | 116 | 939 | 1.29 |
| CO | 205 | 410 | 205 | 205 | 0.51 |
| VOC | 79 | 157 | 79 | 79 | 0.20 |
| PM_{10} | 19 | 39 | 19 | 19 | 0.05 |
| SO_2 | 4 | 8 | 4 | 4 | 0.01 |

| STARTUP SUBTOTAL | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|---------------------|-----------|-----------|-----------|-----------|--------------|
| NO_x | 3,189 | 4,638 | 1,025 | 3,287 | 6.07 |
| CO | 5,730 | 15,588 | 5,056 | 7,147 | 16.76 |
| VOC | 1,662 | 4,446 | 1,281 | 1,785 | 4.59 |
| PM_{10} | 283 | 751 | 218 | 301 | 0.78 |
| SO ₂ | 58 | 154 | 44 | 61 | 0.16 |

| TURBINE TOTAL | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|-----------------|-----------|-----------|-----------|-----------|--------------|
| NO_x | 15,354 | 12,928 | 17,451 | 15,379 | 30.56 |
| CO | 26,785 | 32,585 | 28,173 | 29,859 | 58.70 |
| VOC | 5,790 | 7,302 | 6,629 | 6,847 | 13.28 |
| PM_{10} | 16,300 | 13,690 | 17,789 | 17,568 | 32.67 |
| SO ₂ | 3,383 | 2,841 | 3,692 | 3,646 | 6.78 |

| Alstom CTG and HRSG | lbs/hr | lbs/day | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|---------------------|--------|---------|-----------|-----------|-----------|-----------|--------------|
| NO_x | | | 15,354 | 12,928 | 17,451 | 15,379 | 30.56 |
| CO | | | 26,785 | 32,585 | 28,173 | 29,859 | 58.70 |
| VOC | | | 5,790 | 7,302 | 6,629 | 6,847 | 13.28 |
| PM_{10} | | | 16,300 | 13,690 | 17,789 | 17,568 | 32.67 |
| SO_2 | | | 3,383 | 2,841 | 3,692 | 3,646 | 6.78 |

| BOILER | lbs/hr | lbs/day | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|-----------|--------|---------|-----------|-----------|-----------|-----------|--------------|
| NO_x | 0.68 | 16.3 | 95 | 386 | 97 | 97 | 0.34 |
| CO | 2.29 | 55.0 | 321 | 1301 | 327 | 327 | 1.14 |
| VOC | 0.31 | 7.5 | 44 | 177 | 44 | 44 | 0.15 |
| PM_{10} | 0.58 | 13.9 | 81 | 329 | 83 | 83 | 0.29 |
| SO_2 | 0.08 | 1.9 | 11 | 45 | 11 | 11 | 0.04 |

| Cooling Tower | lbs/hr | lbs/day | | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|---------------|--------|---------|---|-----------|-----------|-----------|-----------|--------------|
| NO_x | | - | - | | | | | |
| CO | 1 | - | - | | | | | |
| VOC | - | - | - | | | | | |
| PM_{10} | 0.681 | 16.35 | | 1,471 | 1,487 | 1,504 | 1,504 | 2.98 |
| SO_2 | | - | - | | | | | |

| TOTAL EMISSIONS - Boiler, GE Turbines, Cooling Tower | | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|--|--|-----------|-----------|-----------|-----------|--------------|
| NOx | | 15,449 | 13,314 | 17,548 | 15,476 | 30.89 |
| CO | | 27,105 | 33,886 | 28,501 | 30,187 | 59.84 |
| VOC | | 5,834 | 7,478 | 6,674 | 6,891 | 13.44 |
| PM_{10} | | 17,852 | 15,507 | 19,376 | 19,155 | 35.95 |
| SO_2 | | 3,395 | 2,886 | 3,703 | 3,657 | 6.82 |

| | g/hp-hr | lbs/hr for 1/2 hr | lbs/day (1/2 hour max) | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
|-----------------|---------|----------------------|---------------------------|-----------|-----------|-----------|-----------|--------------|
| NO _x | 6.9 | 4.31 | 1 4.31 | 54 | 54 | 54 | - 54 | 0.108 |
| CO | 1.34 | 1.67 | 7 1.67 | 10 | 10 | 10 | 10 | 0.021 |
| VOC | 0.25 | 0.31 | 0.31 | 2 | 2 | 2 | 2 | 0.004 |
| PM_{10} | 0.22 | 0.27 | 7 0.27 | 2 | 2 | 2 | 2 | 0.003 |
| SO_2 | - | 0.10 | 0.10 | 1 | 1 | 1 | 1 | 0.00 |

| Fire Pump | | | 300.0 | | | | | |
|-----------|---------|---------------------------------------|--------------|-----------|-----------|-----------|-----------|--------------|
| | | · · · · · · · · · · · · · · · · · · · | lbs/day (1/2 | | · | ſ | 1 | |
| | g/hp-hr | lbs/hr | hour max) | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
| NO_x | 5.2 | 3.44 | 1.72 | 43 | 43 | 43 | 43 | 0.086 |
| CO | 0.27 | 0.18 | 0.09 | 1 | 1 | 1 | 1 | 0.002 |
| VOC | 0.15 | 0.10 | 0.05 | 1 | 1 | 1 | 1 | 0.001 |
| PM_{10} | 0.09 | 0.06 | 0.03 | 0 | 0 | 0 | 0 | 0.001 |
| SO_2 | 0.099 | 0.38 | 0.19 | 2 | 2 | 2 | 2 | 0.005 |

Assuming 30 minutes per week testing (12.5 hours/quarter) and total of 50 hrs per year max at 100% load.

Daily maximum calculated based on 30 minutes testing. Quarterly emissions calculated based on 12.5 hours per quarter.

| Total Facility - Alston | n GX100 Turbines | | | | | |
|-------------------------|------------------|-----------|-----------|-----------|-----------|--------------|
| | | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Annual (Tpy) |
| NO _x | | 15,546 | 13,411 | 17,645 | 15,573 | 31.09 |
| CO | | 27,117 | 33,898 | 28,512 | 30,198 | 59.86 |
| VOC | | 5,836 | 7,481 | 6,676 | 6,894 | 13.44 |
| PM_{10} | | 17,854 | 15,509 | 19,378 | 19,157 | 35.95 |
| SO_2 | | 3,398 | 2,889 | 3,706 | 3,660 | 6.83 |

PCAPCD CALCULATIONS FOR BOILER

PCAPCD Boiler Emission Calculations

Fuel

Density

Natural Gas (lbs/scf) Btu/lb

0.045 22,794 1,026

Boiler Rating

58MMBtu/hr 56,530scf per hour

NOx Calculations (Enter number in cell with blue text)

ppm = 9.24measured

acfm= 16709.6

Mosture Content 16.66%

dscfm=dry standard cubic feet per minute= 10,063

Btu/scf

SV = specific molar volume = 379.5 @ 60 degrees F

Qsd = flowrate dscfm

MW = NOx = 46

NOx lbs/hr = $ppm x 10^-06[MW]/SV x Qsd x 60$ lbs/day

Max 0.68

CO Calculations (Enter number in cell with blue text)

ppm @3%O2 = 50

ppm = 51.31 measured

acfm= 16709.6

Mosture Content 16.66%

dscfm=dry standard cubic feet per minute= 10,063

SV = specific molar volume = 379.5 @ 60 degrees F

Qsd = flowrate dscfm

MW = CO = 28

CO lbs/hr = $ppm x 10^-06[MW]/SV x Qsd x 60$ lbs/day

Max 2.29

VOC Calculations

Emission Factor

(lbs/MMscf) MMscf/hr lbs/hr

5.5 0.056530214 0.311

PM-10 Calculations

District Emission Calculations Factor

using AP-42 (lbs/MMscf)* MMscf/hr lbs/hr

7.6 0.0565302 0.430

* AP-42 (7/98) Table 1.4-2 Emission Factors for Criteria Pollutants and Greenhouse gases from natural gas combustion

Applicant indicates the boiler PM-10 emissions will be 0.01 lbs/MMBtu. At 58 MMBtu/hr, PM-10 emission are calculated by multiplying 58 x 0.01. This equals 0.58 lbs/hr of PM-10.

SOx-10 Calculations

Emission Factor (lbs/MMscf)

> 0.6 for gas with 20 grains per 100 cf* 1.5 for natural gas with 50 grains/100 cf

* AP-42 (7/98) Table 1.4-2 Emission Factors for Criteria Pollutants and Greenhouse gases from natural gas combustion; assumes 100% of fuel sulfur is converted to SO2

> Emission Factor

(lbs/MMscf) MMscf/hr lbs/hr

| | 1.5 | 0.0565 | 0.08 | | | | | |
|-----------|-----|--------|---------|-----------|-----------|-----------|-----------|------------|
| | | | Max/day | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 | Hours/year |
| Operating | | | 24 | 140 | 568 | 143 | 143 | 995 |
| hours | | | | | | | | |

| Boiler | | | | | | | |
|--------|--------|-------------|------------------|------------------|------------------|------------------|--------------|
| | lbs/hr | lbs/day max | Quarter 1 lbs | Quarter 2 lbs | Quarter 3 lbs | Quarter 4 lbs | Annual (Tpy) |
| NOx | 0.68 | 16.3 | 95 | 386 | 97 | 97 | 0.34 |
| СО | 2.29 | 55.0 | 321 | 1,301 | 327 | 327 | 1.14 |
| VOC | 0.31 | 7.5 | 44 | 177 | 44 | 44 | 0.15 |
| PM10 | 0.58 | 13.9 | 81 | 329 | 83 | 83 | 0.29 |
| SO2 | 0.08 | 1.9 | 11 | 45 | 11 | 11 | 0.04 |

Fuel

Density

Natural Gas (lbs/scf)

Btu/lb Btu/scf

0.045 22,794 1,026

Boiler Rating

58MMBtu/hr 56,530scf per hour

APPENDIX E ERC SUMMARY TABLES

| NOx ERC's | for | Roseville | Energy | Park |
|-----------|-----|-----------|--------|------|
|-----------|-----|-----------|--------|------|

| | NOX ERC'S | s for Rose | ville Energ | зу Рагк | | | | | | | | |
|----------------------------------|------------|-------------|-------------|------------|--------------|------------|-------------|--------------|--------------|----------------|-----|-----------------|
| Before Ratios: | (pounds) | | | | | | | | | | | |
| Certificate | Q1 | Q2 | Q3 | Q4 | Total, ppy | Total, tpy | Type | Location | n | | | |
| 2001-23 | 5050 | 5050 | 5050 | 5050 | 20,200 | 10.10 | NOx | Placer | | | | |
| 2001-26 | 33512 | 33512 | 33512 | 33512 | 134,048 | 67.02 | VOC | Placer | | | | |
| EC-209 | 0 | 6888 | 0 | 3542 | 10,430 | 5.22 | NOx | Yolo-So | lano | | | |
| EC-210 | 0 | 10620 | 0 | 4414 | 15,034 | 7.52 | NOx | Yolo-So | lano | | | |
| Energy 2001, | 5300 | 5300 | 5250 | 4150 | 20,000 | 10.00 | NOx | Placer | | | | |
| Inc./SMAQMD Bank | 3300 | 5500 | 3230 | 4130 | 20,000 | 10.00 | NOX | | | | | |
| After Ratios and Y-S I | Hold-Back: | (Certificat | tes for sur | render p | rior to cons | truction) | | NOx Ratio | VOC Ratio | Total Ratio | | -S Hold- ack |
| 2001-23 | 2525 | 2525 | 2525 | 2525 | 10100 | 5.05 | | 2. | 0 | 1.0 | 2.0 | |
| 2001-26 | 6445 | 6445 | 6445 | 6445 | 25778 | 12.89 | | 2. | 0 | 2.6 | 5.2 | |
| EC-209 | 0 | 2952 | 0 | 1518 | 4470 | 2.24 | | 2. | 1 | 1.0 | 2.1 | 0.1 |
| EC-210 | 0 | 4551 | 0 | 1892 | 6443 | 3.22 | | 2. | 1 | 1.0 | 2.1 | 0.1 |
| Subtotals | 8970 | 16473 | 8970 | 12379 | 46792 | 23.396 | | | | | | |
| Target by Quarter | 11,337 | 7,429 | 15,647 | 12,379 | 46,792 | 23.396 | | | | | | |
| From Q1 | 8970 | | | | 8970 | 100.00% | Pct. Of ava | ilable quar | ter cred | its | | |
| From Q2 | 2367 | 7429 | 6677 | | 16473 | 100.00% | | | | | | |
| From Q3 | | | 8970 | | 8970 | 100.00% | | | | | | |
| From Q4 | | | | 12379 | 12379 | 100.00% | | | | | | |
| Quarter Totals | 11,337 | 7,429 | 15,647 | 12,379 | 46,792 | | | | | | | |
| Pct of needed | 100.00% | 100.00% | 100.00% | 100.00% | | | | | | | | |
| After Ratios and Y-S I | Hold-Back: | (Including | g anticipat | ed certifi | cates)) | | | | | | | |
| 2001-23 | 2525 | 2525 | 2525 | 2525 | 10100 | 5.05 | | | | | | |
| 2001-26 | 6445 | 6445 | 6445 | 6445 | 25778 | 12.89 | | | | | | |
| EC-209 | 0 | 2952 | 0 | 1518 | 3 4470 | 2.24 | | | | | | |
| EC-210 | 0 | 4551 | 0 | 1892 | 6443 | 3.22 | | | | | | |
| Energy 2001, Inc./SMAQMD Bank | 4077 | 4077 | 4038 | 3192 | 15385 | 7.69 | | 1. | 3 | 1.0 | 1.3 | |
| Subtotals | 13047 | 20550 | 13008 | 15572 | 62,176 | 31.09 | | | | | | |
| Target by Quarter | 15,546 | 13,412 | 17,646 | 15,572 | 62,176 | 31.09 | | | | | | |
| From Q1 | 13,047 | | | | 13047 | 100.00% | Pct. Of ava | ilable quar | ter cred | its | | |
| From Q2 | 2500 | 13412 | 4638 | | 20550 | 100.00% | | | | | | |
| From Q3 | | | 13008 | | 13008 | 100.00% | | | | | | |
| From Q4 | | | | 15,572 | 15572 | 100.00% | | | | | | |
| Quarter Totals | 15,547 | 13,412 | 17,646 | 15,572 | 62,176 | 62,176 | | | | | | |
| Pct of needed | 100.00% | 100.00% | 100.00% | 100.00% | | • | | | | | | |
| | | | | | | | | | | | | |

PM10 for Roseville Energy Park

13,323

4,200

17,523

100.00%

15,246

15,246

18999

18,999

100.00% 100.00% 100.00%

18,788

18,788

From Q1

From Q2

From Q3

From Q4

Totals

| | ALSTOM TO | JRBINE OF | TION | | | | | | | | | |
|----------------------------------|------------------|------------------|-----------|---------|------------|------------|-------------------------|----------------|---------|------------|--------|--------|
| Before Ratios: | (p | ounds/quai | ter) | | | | | Excess to | be retu | ırned - Al | stom | Option |
| Certificate | Q1 | Q2 | Q3 | Q4 | Total, ppy | Total, tpy | Location | | Q1 | Q2 | Q3 | Q4 |
| 2001-22 | 2,578 | 20,167 | 16,085 | 15,916 | 54,746 | 27.37 | Lincoln, Placer Cou | ınty 2001-22 | 0 | 2,096 | 0 | 0 |
| 2001-24 | 22,680 | - | 13,440 | 22,680 | 58,800 | 29.40 | Forresthill, Placer (| County | | | | |
| 2001-24 (Reissued as 2004-06) | 362 | - | 420 | - | 782 | 0.39 | Forresthill, Placer (| County | | | | |
| Totals | 25,620 | 20,167 | 29,945 | 38,596 | 114,328 | 56.77 | | | | | | |
| After RatiosCertificates for sur | render prior t | o construc | tion | | | | PM10 Ratio | | | | | |
| 2001-22 | 1,983 | 15,513 | 12,373 | 12,243 | 42,112 | 21.06 | 1.3 | | | | | |
| 2001-24 | 11,340 | - | 6,720 | 11,340 | 29,400 | 14.70 | 2.0 | | | | | |
| 2001-24 (Reissued 2004-06) | 181 | - | 210 | | 391 | 0.20 | | | | | | |
| Totals | 13,504 | 15,513 | 19,303 | 23,583 | 71,903 | 35.95 | | | | | | |
| | | | | | | _ | | | | | | |
| Target by Quarter | 17,854 | 15,513 | 19,378 | 19,158 | 71,903 | 35.95 | Excess (Based on GTX10 | 0worst case) | | | | |
| From Q1 | 13,504 | | | | 13,504 | 100.00% | - | | | | | |
| From Q2 | | 15,513 | | | 15,513 | 100.00% | 0.1 | | | | | |
| From Q3 | | | 19,303 | | 19,303 | 100.00% | - | 0.1 | | | | |
| From Q4 | 4350 | | 75 | 19,158 | 23,583 | 100.00% | О | | | | | |
| Totals | 17,854 | 15,513 | 19,378 | 19,158 | 71,903 | | | | | | | |
| | 100.00% | 100.00% | 100.00% | 100.00% | 1 | | 0 | | | | | |
| | PM10 for Re | oseville En | ergy Park | | | | | | | | | |
| | GE TURBIN | IE OPTION | | | | | | | | | | |
| Before Ratios: | (p | oounds) | | | | | | Excess to | be retu | ırned - G | E Opti | on |
| Certificate | Q1 | Q2 | Q3 | Q4 | Total, ppy | Total, tpy | Location | | Q1 | Q2 | Q3 | Q4 |
| 2001-22 | 2,578 | 19,820 | 16,085 | 15,916 | 54,399 | 27.20 | Lincoln, Placer Cou | ınty 2001-22 | 0 | 2,443 | 0 | 0 |
| 2001-24 | 22,680 | - | 13,252 | 21,490 | 57,422 | 28.71 | Forresthill, Placer (| County 2001-24 | 0 | 0 | 188 | 1190 |
| Totals | 25,258 | 19,820 | 29,337 | 37,406 | 111,821 | 55.91 | | | | | | |
| After RatiosCertificates for sur | render prior t | o construc | tion | | | | PM10 Ratio | | | | | |
| 2001-22 | 1,983 | 15,246 | 12,373 | 12,243 | 41,845 | 20.92 | 1.3 | | | | | |
| 2001-24 | 11,340 | - | 6,626 | 10,745 | 28,711 | 14.36 | 2.0 | | | | | |
| Totals | 13,323 | 15,246 | 18,999 | 22,988 | 70,556 | 35.28 | | | | | | |
| Target by Quarter | 17,523 | 15,246 | 18,999 | 18,788 | 70,556 | 35.28 | Excess (Based on LM600) | 0) | | | | |
| _ ~ ~ | | • | - | • | | | _ ` | • | | | | |

13,323 100.00%

15,246 100.00%

18,999 100.00%

22,988 100.00%

70,556

0

APPENDIX F

LETTER FROM APPLICANT ON INTERPOLLUTANT TRADING RATIO

John Finnell
Sr. Air Pollution Control Engineer
Placer County APCD
11464 B Avenue
DeWitt Center
Auburn, Ca. 95603

Subject: Roseville Energy Park VOC or NO_x Interpollutant Trading Ratio

Dear Mr. Finnell;

Roseville Electric (RE) is proposing to use VOC emission reduction credits to offset a portion of their NO_x emissions from the proposed Roseville Energy Park (REP). They are proposing a 2.6:1 interpollutant offset ratio that, when applied to the Placer County APCD distance ratio of 2.0, results in a final ratio of 5.2:1. The proposed use of the 2.6:1 offset ratio is based upon review of the SMUD Cosumnes Power Project (CPP) interpollutant trade analysis, dated October 21, 2002. CPP performed a wide variety of analyses, including the use of the UAM model, to determine a VOC/NO_x offset ratio. These results of the UAM modeling are summarized in the October 21, 2002 Final Determination of Compliance. These studies indicate that a large degree of uncertainty exists with each method used to calculate interpollutant offset ratios. The UAM results provide a range of offset ratios between 0.6 and 7.9 with an average VOC/NO_x ratio of 2.0:1. To account for model uncertainty, an additional factor of 30% was applied to the average VOC/NO_x ratio to produce a final ratio of 2.6:1. REP proposes to use the same conservative 2.6:1 VOC/NO_x ratio rather than performing new UAM analyses that would ultimately produce a similar range of uncertainties. Furthermore, it is RE's position that the regional climate of the greater Sacramento area controls the generation of ozone.

Ozone formation depends on many factors but in the Sacramento area, the two most important factors are mobile emissions and weather conditions. Although changes in regional daily emissions of ozone precursors (such as automobile emissions) can affect daily ozone concentrations, weather variations best explain the day-to-day changes in ozone concentrations in this region. Understanding how weather influences ozone concentrations is critical in accurately predicting high ozone concentrations.

RE's proposal to use the CPP UAM study in order to apply the 2.6:1 interpollutant offset ratio is based on the fact that similar meteorological patterns exist between the REP and CPP sites that produce high ozone days. The proposed REP and CPP project sites are both situated in a transition zone between the Sierra Nevada Mountains and the Central Valley

of California, within the Sacramento Valley. In this area, broad alluvial fans extend from the Sierra Nevada Mountains in the east toward sedimentary deposits in the Sacramento Valley to the west. A regional location map is shown in the attached figure that also includes the location of the CPP project in relation to REP.

The terrain in the vicinity of REP and CPP is characterized as generally flat with rolling foothills and the Sierra Nevada Mountains to the east, and the Sacramento Valley extending to the north, west and south. The terrain elevation on the REP plant site is approximately 95 feet above mean sea level (amsl). The proposed REP project is located in Placer County, in the southern part of the Sacramento Valley Air Basin while the CPP project site is located in South Sacramento County at an elevation of 160 feet (amsl). The overall terrain in the vicinity of both projects slopes gently downward in a westward direction toward the Sacramento Valley. At present, the area surrounding the site is generally undeveloped with some agricultural land uses.

The overall climate of California and including the REP and CPP project areas is "Mediterranean," with overall moderate annual temperatures and precipitation occurring primarily during the winter months. The meteorology is dominated by a semi-permanent high-pressure system over the eastern Pacific Ocean off the coast of California. The center of the high-pressure system varies northward and southward. Its position strongly influences the weather in the region.

Given the large spatial variation of the primary emissions within the greater Sacramento area, it is the local regional climate that fosters generation of ozone. Meteorology is the dominant factor controlling the change in ozone air quality from one day to the next. Synoptic and mesoscale meteorological features govern the transport of emissions between sources and receptors, affecting the dilution and dispersion of pollutants during transport and the time available during which pollutants can react with one another to form ozone. These features are important to transport studies and modeling efforts owing to their influence on reactive components and ozone formation and deposition.

The summer climatology of central California is generally dominated by the semipermanent Eastern Pacific High-Pressure System. This synoptic feature is manifest as a dome of warm air (a maximum in the 500-mb geopotential height field) with a surrounding anticyclonic circulation (clockwise in the Northern Hemisphere). Therefore, surface winds blow clockwise and outward from the high, a motion associated with low-level divergence, and therefore sinking motion aloft and fair weather. This sinking motion also gives rise to adiabatic heating and therefore warm temperatures aloft. A key indicator of this warm, capping subsidence inversion in California is the temperature of the 850-mb pressure surface from the Oakland soundings. This single meteorological variable from the 0400 PST sounding is perhaps best correlated with surface ozone concentrations in the central valley (e.g., Smith et al. 1984; Smith 1994; Fairley and De Mandel 1996, Ship and McIntosh 1999). The shape of the 500-mb height contours (at 5500-m elevation) over the Eastern Pacific is broad and flat and can extend inland for hundreds of kilometers.

Accompanying the warm temperatures aloft, are warm temperatures on the central valley floor. The coastal cities of San Francisco and Santa Maria have mean daily maximum temperatures in the low- to mid-70s (deg F) while Sacramento averages about 20 F warmer. The northern and southern ends of the Central Valley, represented by Redding and Bakersfield, average an additional 5 F warmer than Sacramento. This heating causes an inland thermal low pressure trough as evidenced by the lower station pressures at Redding and Bakersfield. The pressure gradient enhances the movement of the thermally generated sea breeze through the Carquinez Straight, through other gaps in the coastal range to the north and south of the San Francisco Bay, and sometimes over the coastal range altogether. Pollutants from the San Francisco Bay Area source region are carried with the breeze to receptor regions within the Central Valley. With the abundant sunlight accompanying this weather pattern, the transported pollutants and the Sacramento Valley and San Joaquin Valley emissions cause frequent exceedances of the 1hr and 8hr standards at several sites in the interior of the Central Valley.

This typical scenario is observed on most summer afternoons. For the San Francisco Bay Area, Hayes et al. (1984) assign a frequency of 77% to sea breeze conditions matching average surface wind streamlines at 1600 PST. They give a frequency of 75% for the Sacramento Valley. However, the high pressure system can migrate with changes in the planetary weather pattern. The center of the pressure cell can move ashore, causing a decrease and even a reversal in the mean pressure gradients (Pun et al. 1998). The sea breeze is weakened, and its inland extent can become limited, leading to stagnation conditions fostering higher ozone concentrations in many areas. The high can also move east all together, followed by a trough that ventilates the valley. The high pressure is not always dominant. Neff et al. (1994) classified synoptic patterns during summer 1994 and found approximately one-third of the days to be "normal" Pacific highs, one-third to be inland highs, and one-third to be troughs. Therefore, the mesoscale sea breeze surface pattern, with 77% frequency, must exist in more than one synoptic regime. Mesoscale features must be considered in any discussion of ozone climatology. Several mesoscale flow features in Central California can have significant air quality impacts by transporting or blocking transport of ozone and precursors between important source/receptor couples. These are discussed below.

The Sea Breeze and Marine Air Intrusion

Differential heating between the land and ocean causes a pressure gradient between the relatively cooler denser air over ocean and the warmer air over the land. The marine air mass comes ashore. However, this heating takes time to occur and may be impeded if a cloud cover prevents direct insolation of the land. A further complication may be provided by any additional surface pressure gradients due to synoptic conditions that can enhance, hinder, or overwhelm this thermal effect. The actual time of onset of a sea breeze can be difficult to forecast with overnight fog or coastal status. Typically, with calm coastal mornings, rush hour pollutants can accumulate in the coastal source region. Then, as the sea breeze is established (often by late-morning, usually by mid-day), maximum ozone production can occur after pollutants leave the coastal areas. It is well-known that maximum ozone occurs downwind of respective source areas (e.g., Livermore downwind of the San Francisco Bay communities.) As marine air penetrates the mainland, it is modified and can become entrained in a different thermal flow, e.g., an upvalley or upslope flow. Studies of sea breeze and marine air intrusion

impacts on Central California air quality include that by Stoeckenius et al, (1994), who present an objective classification scheme.

Nocturnal Jets and Eddies

A low-level nocturnal wind maximum can arise as the nocturnal inversion forms and effectively reduces boundary layer friction. Wind friction can be represented as a force that is directly opposed to the wind (termed the "antitriptic wind" by Schaefer and Doswell 1980). The overall direction of flow is determined by the vector balance among horizontal pressure gradient, Coriolis, and frictional forces. However, in the evening, with the establishment of a surface-based nocturnal inversion, the friction is "turned off." The flow is no longer in balance, and there is a component of the pressure gradient force that is directed along the wind, increasing wind speed, which increases the Coriolis force. Since Coriolis force is always 90° to the right of the wind (in the northern hemisphere), this means that the wind must veer. In the San Joaquin Valley, the rapidly moving jet (7-30 m/s) may veer toward the western valley but is channeled by the topography and soon encounters the Tehachapi range. While the nocturnal jet may be present in other seasons, it has been observed during the ozone season (Smith et al. 1981). It is believed to be a transport mechanism during the summer months. Depending on the temperature structure of the valley, the jet may not be able to exit through Tehachapi Pass (~1400 meters), as it can during the neutral stability of daytime convective heating. The air is forced to turn north along the Sierra foothills at the southeastern edge of the San Joaquin Valley. During the Southern San Joaquin Ozone Study, Blumenthal et al. (1985) measured the Fresno eddy extending above 900 meters amsl about 50% of the time. The impact of these jets and eddies is to redistribute pollutants within an air basin. The San Joaquin Valley nocturnal jet can bring pollutants from the north part of the valley to the south overnight. Ozone created in the south San Joaquin Valley can then be redistributed to the central San Joaquin Valley and/or can be transported into layers aloft by the eddy. The Schultz eddy forms when westerly marine air flow in the south San Joaquin Valley (which may become a jet with the evening boundary layer) impacts the Sierra and turns north. It can redistribute pollutants to Sutter Buttes and points north and east (or west after a half-circulation) of Sacramento (Schultz, 1975; ARB, 1989).

<u>Upslope/Downslope Flow</u>

The increased daytime heating in mountain canyons and valleys with a topographic amplification factor (i.e., heating less air volume when compared to flat land; see White, 1991) causes significant upslope flows during the afternoons in the San Joaquin and Sacramento Valleys. This can act as a removal mechanism, and can lift mixing heights on edges of the valleys, relative to the mixing heights at valley center. Myrup et al. (1989) studied transport of aerosols from the San Joaquin valley into Sequoia National Park. They found a net up flow of most species. The return flow can bring pollutants back down. Smith et al. (1981) from tracer mass budgets during tracer releases has estimated pollutant budgets due to slope flow fluxes (and other ventilation mechanisms). Smith et al. caution that less polluted air at higher elevations is entrained in the slope flow, thus diluting San Joaquin Valley air and removing less pollutants. From the tracer mass balance, they found that northwesterly flow

was a more effective dilution mechanism, and the benefits of slope flow removal by upslope flows would be confined to the edges of the valley.

<u>Up-Valley/Down-Valley Flow</u>

Up-valley flow draws air south in the San Joaquin Valley and north in the Sacramento Valley during the day, while down-valley drainage winds tend to ventilate both valleys at night.

Conclusion

The spatial pattern of ozone exceedances is associated with the frequency of particular meteorological conditions that affect transport of pollutants from the major urban centers (i.e., San Francisco Bay Area and Sacramento) to the San Joaquin Valley, Sacramento Valley and to the Mountain Counties. This analysis showed the importance of the sea breeze in determining spatial distribution of ozone accumulation. When the sea breeze is inhibited, higher ozone levels occur throughout the region. In addition, it demonstrates that ozone impacts in the Sacramento area are caused by regional meteorological conditions that exist over large length scales. Thus, regional ozone impacts are a direct consequence of the mesoscale meteorological patterns that exist in region, rather than the specific location of sources of NO_x and VOCs. Both the CPP and REP are located in similar atmospheric and surface geological terrains and thus are subjected to similar meteorological conditions.

The CPP UAM modeling domain included these same meteorological parameters that would simulate the mesoscale patterns that are the driving force in producing high ozone days. Since these mesoscale parameters are of sufficient length scales to incorporate the REP and CPP impact areas, the CPP UAM modeling is applicable to the REP project. With the relatively close proximity of REP to CPP and given that the meteorological modeling domain is of sufficient length scale, review of the CPP UAM modeling analysis shows that the same regional meteorological patterns input into UAM would exist over the Placer County Air Basin, thus, making the existing UAM modeling study applicable to REP in terms of magnitude and scope.

With the application of the Placer County APCD 2.0 distance ratio, which also accounts for the spatial separation of sources, to the 2.6:1 VOC/NO_x ratio from CPP, the resulting offset ratio is 5.2:1. Therefore, based on the fact that regional meteorology is the driving force in producing high ozone concentrations and that the same mesoscale meteorological conditions exist at both the CCP and REP sites, REP proposes to use an overall VOC to NO_x ratio of 5.2:1 for currently identified VOC to NO_x conversions. This VOC/NO_x ratio would produce the highest offset ratio used for any power plants in the state.

If you have any questions or comments, please do not hesitate to call me at (805) 569-6555.

Sincerely,

ATMOSPHERIC DYNAMICS, INC.

Gregory Darvin

Gregory Darvin

APPENDIX G LETTERS REGARDING OFFSETS



October 20, 2004

Mr. Charles Schneider Enron North America Corp. 1221 Lamar Houston, Texas, 77010-1221 Phone (713)-853-1789 **UPS OVERNIGHT**

Subject: Transfer of Emission Reduction Credits

Dear Mr. Schneider:

The District has completed the transfer of Emission Reduction Credit (ERCs) which was requested in your October 12, 2004 letter. ERC Certificate Number 2001-23, 2002-26, 2001-22 have been transferred in full to the City of Roseville. A portion of ERC Certificate Number 2001-24 was transferred to the City of Roseville. The balance was reissued to Enron North America as shown below:

| | Quarter 1 | Quarter 2 | Quarter 3 | Quarter 4 |
|--------------------------------|-----------|-----------|-----------|-----------|
| From Enron North America | 50,676 | 50,676 | 50,676 | 50,676 |
| ERC Certificate 2001-24 | | | | |
| To City of Roseville | 22,680 | 0 | 13,440 | 22,680 |
| ERC Certificate 2004-04 | | | | |
| Balance to Enron North America | | | | |
| ERC Certificate 2004-06 | 27,996 | 50,676 | 37,236 | 27,996 |

All certificates are enclosed per your request. An Enron North America representative must sign ERC Certificate 2004-06 and return a copy to the District. The certificates which were transferred to the City of Roseville are to be signed by them upon receipt. Please contact me at (530) 889-7133 if you have any questions.

Sincerely,

John Finnell Sr. Air Pollution Control Engineer

Encl: ERC Certificates #2004-02, 2004-03, 2004-04, 2004-05 and 2004-06



Thomas J. Christofk, Air Pollution Control Officer

EMISSION REDUCTION CREDIT

CERTIFICATE No. 2004-02

(Reference No. 2001-20 and 2001-22)

IS HEREBY ISSUED TO

City of Roseville 2090 Hilltop Circle Roseville, CA 95677

FOR ACTUAL EMISSION REDUCTIONS CREATED AT

RC Collett, Inc. 1800 Sunset Blvd., Rocklin, CA 95677

EMISSIONS UNITS: Aggregate Plant

THE FOLLOWING EMISSION REDUCTIONS (IN POUNDS PER QUARTER) ARE HEREBY GRANTED PURSUANT TO DISTRICT RULE 504:

POLLUTANT <u>1st QTR 2nd QTR 3rd QTR 4th QTR</u> Fine Particulate (PM-10) 2,578 22,263 16,085 15,916

SUBJECT TO THE FOLLOWING CONDITIONS

- 1. The issuance of this ERC certificate shall not constitute evidence of compliance with the rules and regulations of the District, or a representation or assurance to the recipient upon which reliance is authorized or intended that the ERC represented by the ERC certificate are available from the District ERC bank.
- 2. Upon transfer of ERC's between parties, the transferor's ERC certificate, and a copy of an agreement, signed by the transferor, authorizing and memorializing the transfer of the ERC to the transferee must be surrendered to the Air Pollution Control Officer by the transferee, within 30 days of the date of the agreement authorizing the transfer of the ERC's.

| DAT | E ISSUED: 11/9/2004 | |
|-----|-------------------------------|-----------------------------------|
| | | SIGNATURE, OWNER'S REPRESENTATIVE |
| BY: | | |
| | THOMAS J. CHRISTOFK | PRINTED NAME OF SIGNATORY |
| | AIR POLLUTION CONTROL OFFICER | |
| | | TITLE |

[U:\APC\ERC REGISTER\ERC FILES\2004_02.DOC]



Thomas J. Christofk, Air Pollution Control Officer

EMISSION REDUCTION CREDIT

CERTIFICATE No. 2004-03 (Reference No. 2001-02, 2001-12, 2001-23)

IS HEREBY ISSUED TO City of Roseville 2090 Hilltop Circle Roseville, CA 95677

FOR ACTUAL EMISSION REDUCTIONS CREATED AT

Georgia-Pacific Corporation 23801 Foresthill Road Foresthill, California 95631

EMISSIONS UNIT: SAWMILL WITH TWO WOODWASTE FIRED BOILERS

THE FOLLOWING EMISSION REDUCTIONS (IN POUNDS PER QUARTER) ARE HEREBY GRANTED PURSUANT TO DISTRICT RULE 504:

 POLLUTANT
 1st QTR
 2nd QTR
 3rd QTR
 4th QTR

 NITROGEN OXIDES
 5,050
 5,050
 5,050
 5,050

- 1. The issuance of this ERC certificate shall not constitute evidence of compliance with the rules and regulations of the District, or a representation or assurance to the recipient upon which reliance is authorized or intended that the ERC represented by the ERC certificate are available from the District ERC bank.
- 2. Upon transfer of ERC's between parties, the transferor's ERC certificate, and a copy of an agreement, signed by the transferor, authorizing and memorializing the transfer of the ERC to the transferee must be surrendered to the Air Pollution Control Officer by the transferee, within 30 days of the date of the agreement authorizing the transfer of the ERC's.

| DAT | E ISSUED: October 20, 2004 | |
|-----|--|-----------------------------------|
| | | SIGNATURE, OWNER'S REPRESENTATIVE |
| BY: | | |
| | THOMAS J. CHRISTOFK AIR POLLUTION CONTROL OFFICER | PRINTED NAME OF SIGNATORY |
| | | TITLE |



Thomas J. Christofk, Air Pollution Control Officer

EMISSION REDUCTION CREDIT

CERTIFICATE No. 2004-04

(Reference No. 2001-03, 2001-13, 2001-24)

IS HEREBY ISSUED TO City of Roseville 2090 Hilltop Circle Roseville, CA 95677

FOR ACTUAL EMISSION REDUCTIONS CREATED AT

Georgia-Pacific Corporation 23801 Foresthill Road Foresthill, California 95631

EMISSIONS UNIT: SAWMILL WITH TWO WOODWASTE FIRED BOILERS

THE FOLLOWING EMISSION REDUCTIONS (IN POUNDS PER QUARTER) ARE HEREBY GRANTED PURSUANT TO DISTRICT RULE 504:

POLLUTANT <u>1st QTR 2nd QTR 3rd QTR 4th QTR</u> **FINE PARTICULAT (PM-10)** 22,680 0 13,440 22,680

- 1. The issuance of this ERC certificate shall not constitute evidence of compliance with the rules and regulations of the District, or a representation or assurance to the recipient upon which reliance is authorized or intended that the ERC represented by the ERC certificate are available from the District ERC bank.
- 2. Upon transfer of ERC's between parties, the transferor's ERC certificate, and a copy of an agreement, signed by the transferor, authorizing and memorializing the transfer of the ERC to the transferee must be surrendered to the Air Pollution Control Officer by the transferee, within 30 days of the date of the agreement authorizing the transfer of the ERC's.

| DAT | E ISSUED: October 20, 2004 | |
|-----|--|-----------------------------------|
| | | SIGNATURE, OWNER'S REPRESENTATIVE |
| BY: | | |
| | THOMAS J. CHRISTOFK AIR POLLUTION CONTROL OFFICER | PRINTED NAME OF SIGNATORY |
| | | TITLE |



Thomas J. Christofk, Air Pollution Control Officer

EMISSION REDUCTION CREDIT CERTIFICATE No. 2004-05

(Reference No. 2001-05, 2001-15, 2001-26)

IS HEREBY ISSUED TO City of Roseville 2090 Hilltop Circle Roseville, CA 95677

FOR ACTUAL EMISSION REDUCTIONS CREATED AT

Georgia-Pacific Corporation 23801 Foresthill Road Foresthill, California 95631

EMISSIONS UNIT: SAWMILL WITH TWO WOODWASTE FIRED BOILERS

THE FOLLOWING EMISSION REDUCTIONS (IN POUNDS PER QUARTER) ARE HEREBY GRANTED PURSUANT TO DISTRICT RULE 504:

POLLUTANT <u>1st QTR 2nd QTR 3rd QTR 4th QTR</u> VOLATILE ORGANIC COMPOUNDS 33,512 33,512 33,512

- 1. The issuance of this ERC certificate shall not constitute evidence of compliance with the rules and regulations of the District, or a representation or assurance to the recipient upon which reliance is authorized or intended that the ERC represented by the ERC certificate are available from the District ERC bank.
- 2. Upon transfer of ERC's between parties, the transferor's ERC certificate, and a copy of an agreement, signed by the transferor, authorizing and memorializing the transfer of the ERC to the transferee must be surrendered to the Air Pollution Control Officer by the transferee, within 30 days of the date of the agreement authorizing the transfer of the ERC's.

| DAT | E ISSUED: October 20, 2004 | |
|-----|--|-----------------------------------|
| | | SIGNATURE, OWNER'S REPRESENTATIVE |
| BY: | | |
| | THOMAS J. CHRISTOFK AIR POLLUTION CONTROL OFFICER | PRINTED NAME OF SIGNATORY |
| | | TITLE |



Thomas J. Christofk, Air Pollution Control Officer

EMISSION REDUCTION CREDIT

CERTIFICATE No. 2004-06 (Reference No. 2001-03, 2001-13, 2001-24)

IS HEREBY ISSUED TO
Enron North America
P.O. Box 1188
Houston, Texas 77251-1188

FOR ACTUAL EMISSION REDUCTIONS CREATED AT

Georgia-Pacific Corporation 23801 Foresthill Road Foresthill, California 95631

EMISSIONS UNIT: SAWMILL WITH TWO WOODWASTE FIRED BOILERS

THE FOLLOWING EMISSION REDUCTIONS (IN POUNDS PER QUARTER) ARE HEREBY GRANTED PURSUANT TO DISTRICT RULE 504:

POLLUTANT <u>1st QTR 2nd QTR 3rd QTR 4th QTR</u> PM-10 27,996 50,676 37,236 27,996

- 1. The issuance of this ERC certificate shall not constitute evidence of compliance with the rules and regulations of the District, or a representation or assurance to the recipient upon which reliance is authorized or intended that the ERC represented by the ERC certificate are available from the District ERC bank
- 2. Upon transfer of ERC's between parties, the transferor's ERC certificate, and a copy of an agreement, signed by the transferor, authorizing and memorializing the transfer of the ERC to the transferee must be surrendered to the Air Pollution Control Officer by the transferee, within 30 days of the date of the agreement authorizing the transfer of the ERC's.

| DAT | E ISSUED: October 20, 2004 | |
|-----|--|-----------------------------------|
| | | SIGNATURE, OWNER'S REPRESENTATIVE |
| BY: | | |
| | THOMAS J. CHRISTOFK AIR POLLUTION CONTROL OFFICER | PRINTED NAME OF SIGNATORY |
| | | TITLE |



P.O. Box 1188 Houston, TX 77251-1188

February 25, 2004

Mr. Tom Habashi Electric Utility Director City of Roseville 2090 Hilltop Circle Roseville, California 95747

Re: Purchase and Sale of Emission Reduction Credits

Dear Mr. Habashi:

Pursuant to your request, this letter confirms that Enron North America Corporation ("Enron") and the City of Roseville ("Roseville") recently executed a Purchase and Sale Agreement dated as of February 13, 2004 (the "Agreement") for the purchase and sale of certain emission reduction credits ("ERC's"). As of the date of the Agreement, and subject to the terms and conditions set forth in said Agreement, Enron agrees to sell and Roseville undertakes to buy the following ERC's:

| Placer County Air Pollution Control District Certificate # | Pollutant | Quantity (tons/year) |
|--|-----------|-------------------------|
| 2001-23 | NOx | 10.1 |
| 2002-26 | VOC | 67.0 |
| 2001-22 | PM10 | 28.4 |
| 2001-24 | PM10 | 29.4 |

Should you have any questions or concerns regarding the above, please do not hesitate to contact Scott Churbock at 713-345-4623.

Sincerely,

Charles E. Schneider RMP

Managing Director



2090 Hilltop Circle Roseville, CA 95747 Office (916) 774-5600 FAX (916) 784-3797 TDD (916) 774-5220 www.RosevilleElectric.org

May 4, 2004

Mr. Tom Christofk Air Pollution Control Officer Placer County Air Pollution Control District 11464 B Avenue Dewitt Center Auburn, CA 95603

Subject:

Roseville Energy Park

Disclosure of Confidential Emission Reductions

Dear Mr. Christofk,

Roseville Electric has been diligently pursuing securing emission reductions for use as offsets for the Roseville Energy Park (REP). We had previously submitted information to Placer County Air Pollution Control District (District) to support your analysis and preparation of the Determination of Compliance (DOC). Some of the information previously submitted identified holders of Emission Reduction Credits (ERCs) and owners of facilities that may create new ERCs with whom Roseville Electric was negotiating. The District agreed to treat this information as confidential pursuant to state and federal law. At this time, Roseville Electric has concluded negotiations with two emission reduction sources. Since these negotiations have concluded, the District would no longer have to treat the information about these two sources as confidential. We are currently negotiating with others to obtain additional emission reductions and therefore request that the District continue to treat any information previously submitted, other than information relating to the two sources outlined in the attachment to this letter as confidential.

Sincerely,

Robert Hren

REP Project Manager



Roseville Energy Park Additional NOx ERC's

I. Existing ERC's. Roseville Electric and the City of Roseville have concluded negotiations for the following NOx emission reduction credits (ERC's) that are currently held by Calpine Corporation and are banked in the Yolo-Solano Air Quality Management District (YSAQMD):

| | (units: pounds per quarter) | | | |
|---------------------|-----------------------------|--------|----|-------|
| ERC Certificate No. | Q1 | Q2 | Q3 | Q4 |
| EC-209 | 0 | 6,888 | 0 | 3,542 |
| EC-210 | 0 | 10,620 | 0 | 4,414 |

Roseville Electric will be requesting that the interdistrict transfer of these ERC's, for application to the Roseville Energy Park in Placer County, be placed on the District Board agenda for YSAQMD on June 9, 2004 and for PCAPCD on June 10, 2004.

II. New ERC's. The City of Roseville has entered into agreements with Energy 2001, Inc. which include an option to purchase at least 10 tons of new NOx ERC's that may be created at the existing Lincoln Landfill, located within Placer County. Energy 2001, Inc. is currently constructing a power generation facility at the landfill, replacing existing power generators. After the replacement generators are in service, additional control equipment could be installed to reduce NOx emissions and result in certification of new NOx ERC's. It is anticipated that the new NOx ERC's will be certified before the Roseville Energy Park enters commercial operation.



Thomas J. Christofk, Air Pollution Control Officer www.placer.ca.gov/apcd

May 6, 2004

Mr. Robert Hren, REP Project Manager Roseville Electric 2090 Hilltop Circle Roseville, CA95747

Subject: Emission Reduction Credits

Dear Mr. Hren:

The District has received your letter regarding the disclosure of confidential emission reductions for the Roseville Energy Park project. The two emission reduction credit (ERC) certificates, EC-209 and EC-210, issued by Yolo-Solano AQMD (YSAQMD), identified will no longer be treated as confidential and will be identified in the Preliminary Determination of Compliance (PDOC) after staff have reviewed YSAQMD's background documentation on these ERCs.

The attachment to your letter, Item II., New ERCs, discussed potential ERCs from the landfill gas power generators which are being constructed by Energy 2001. This source operated an engine for a very limited time and shut the engine down more than a year ago. Energy 2001 has been issued an Authority to Construct to install two engines. We have not received a notification of completion of construction and presume the engines have not been installed or operated.

District Rule 504, Emission Reduction Credits, identifies the process for quantifying and certifying emission reductions for use of offsets. As stated in the Rule 504, Section 301, only actual emission reductions shall be certified as ERCs. At this time, there are no documented actual emissions reductions at Energy 2001 which could be certified ERCs under Rule 504. The District does not consider emission reductions which might be certified at some future date a viable source of offsets for the Roseville Energy Park.

We do recognize that Roseville Electric is continuing efforts to secure additional ERCs for offsets. Those credits which have been obtained will be discussed in the PDOC. The PDOC will indicate that that there may be shortfall of offsets and the identification of additional ERC certificates for offsets are required <u>before</u> we can prepare a final Determination of Compliance. This must include the ERC certificate number, quantities for each quarter, location of the source of ERCs, and distance of source of ERCs from the Roseville Energy Park.

You might consider other options including reducing the design capacity and resulting emissions from the project or reducing the hours of operation and resulting emissions to the extent that offsets are available at this time.

Letter to Roseville Electric May 6, 2004 Page 2

As you are aware, any ERCs which are to be transferred from outside the District do need to be approved by both District Boards pursuant to the California Health and Safety Code Section 40709.6, Offset by Reductions Credited to Stationary Source Located in Another District. This approval must be obtained prior to the District's issuance of a final Determination of Compliance.

We have scheduled an agenda item this matter for the June 10, 2004 District Board meeting. All available ERCs which are to be transferred should be identified along with a justification for approval under Section 40709.6. This information is needed by no later than May 21, 2004 so that we may prepare the Board package. If not available at that time, the next Board meeting is scheduled for August. Please be aware that failure to obtain approval or delaying approval of interdistrict transfer of ERCs will delay or prevent the issuance of the final Determination of Compliance.

Please contact me at (530) 889-7133 if you have any questions.

Sincerely,

John Finnell Sr. Air Pollution Control Engineer

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